

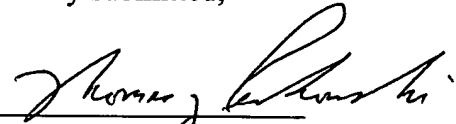
REMARKS

The proposed Amendments to the Specification have been provided to ensure correspondence between the Specification and the Formal Drawings filed herewith.

The Commissioner is hereby authorized to charge any fee deficiencies or credit any overpayments to Deposit Account 16-1340.

Respectfully submitted,

Dated: July 16, 2004




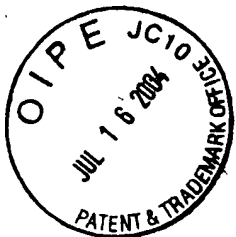
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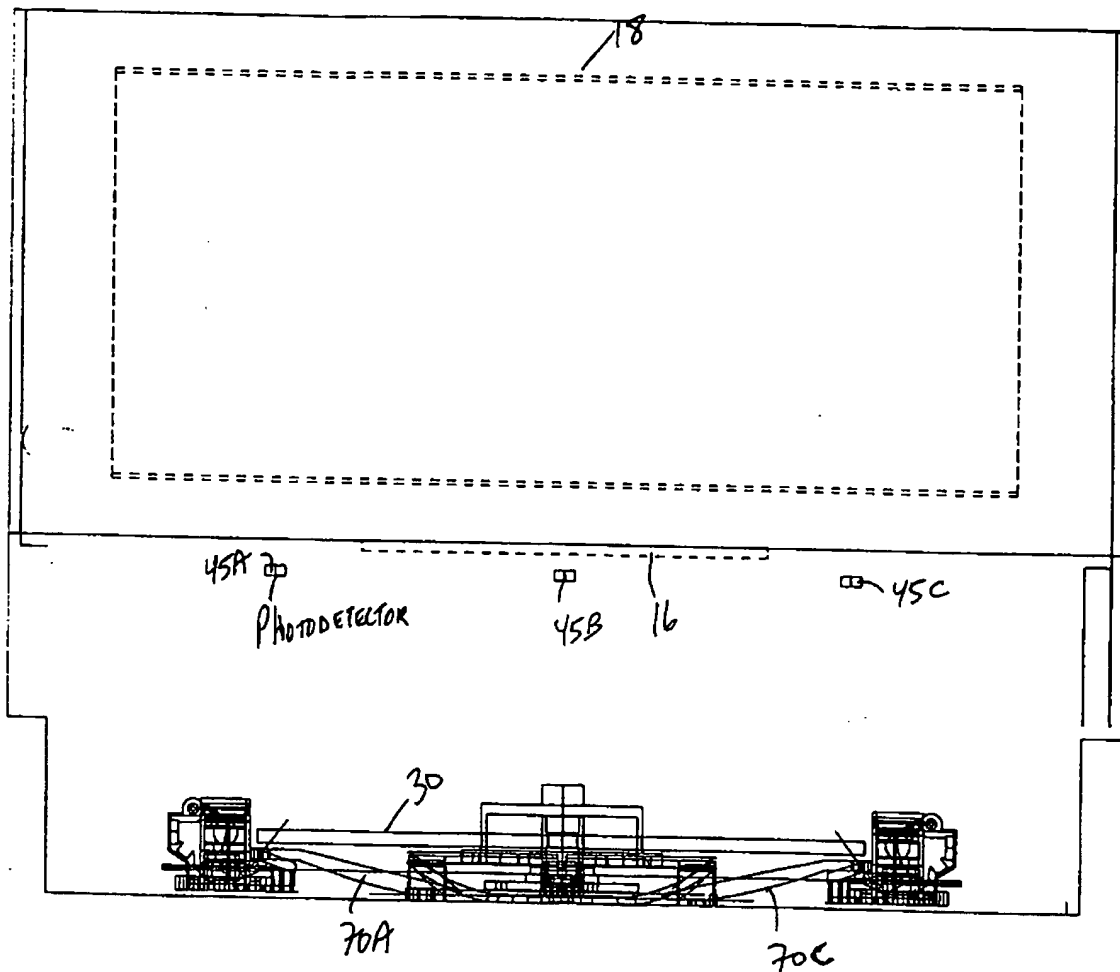
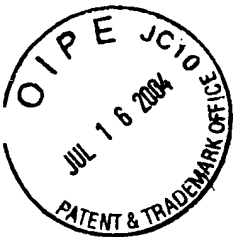


FIG. 2I1
2I



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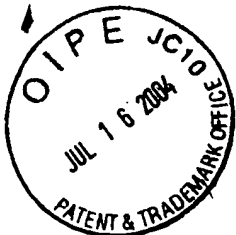
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Table of	Dependent Parameters for both the Scanner and the Disk	Disk	Problem items are highlighted (red)
Box height (inches):	N/A	(See Note 1)	
Box width (inches):	N/A	(See Note 2)	
Max angle B (degrees):	62.00	(See Note 3)	
Min angle B (degrees):	38.00	(See Note 3)	
Total facet angular sweep (degrees):	358.14	(See Note 4)	
Min (angle A - angle B) (degrees):	0.00	(See Note 6)	
Max beam speed (inches per second):	13704		
Min beam speed (inches per second):	7158		
Power at data detector (mW):	872		
Signal voltage (volts):	5.47	(See Note 7)	
Signal voltage at max DOF limits (volts):	3.45	(See Note 7)	
CDRH: P-avg. Class 2? Class 2A?	P-pulse Class 1? YES		0.91 Max bandwidth (MHz) for 7.5 mil bars
IEC: Single pulse PASS	Pulse train correction PASS	(See Note 8)	
Note 1: If this entry is highlighted (red) then the value exceeds the specified value for the box height (Cell G21). Go to cells G417 to G456 to identify the problem entries and make the necessary inner radius adjustments in Cells G215 to G254.			
Note 2: This entry is not used in the box design, but it gives an indication of the box dimensions that would be established by the width of the tops of the mirrors.			
Note 3: Generally, the B angles should range between 40 degrees and 70 degrees. Holograms with smaller or larger angles may be difficult to construct.			
Note 4: This entry must be less than, but within a few degrees of, 360 degrees. To satisfy this requirement, it may be necessary to make adjustments to the focal distances and/or the length of the scan lines.			
Note 6: This value must be greater than 0.5 degrees to avoid feedback into the laser from disk surface reflections. If it is too small, adjustments must be made to the B angles of the problem facets (See Cells X468 to X507).			
Note 7: The signal voltage must be greater than some value established by the signal processor requirements. Typically, this value should be greater than 2 volts. If this value is less than 2 volts, either the laser power must be increased or the focal distances must be decreased.			
Note 8: All CDRH/IEC entries must be YES or PASS. If not, laser power must be reduced. (Modify laser power in Cell B788.)			

FIGS. 3F1 and 3F2



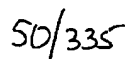
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C. ak.

d = distance from disk to base of scanner (inches):													
Rotational speed of disk (rpm)													
Disk/Stratos 4.21e													
Facet	Diffraction	Focal length (inches)	Geometrical	Angle A (degrees)	Angle B (degrees)	Angle of Diffraction (degrees)	Focal plane scan length (inches)	Scan Angle (degrees)	Scan mult. Factor (m)	Rotation Angle (degrees)	Accounting for dead time for laser beam (degrees)	Light Collection Factor	Maximum Collection Area (ignoring notch) (sq. in.)
1	12.5	12.73		52	38.00	52.00	9.750	42.61	1.62	26.24	27.39	1.00	2.28
2	11.5	11.68		52	40.00	50.00	9.750	45.95	1.62	28.35	29.50	0.80	1.81
3	12.7	12.94		52	42.00	48.00	9.750	42.00	1.58	28.66	27.81	0.92	2.09
4	11.5	11.68		52	44.00	46.00	9.750	45.95	1.57	29.19	30.34	0.71	1.62
5	12.7	12.94		52	46.00	42.00	9.750	42.00	1.50	27.97	29.12	0.79	1.79
6	12.0	12.21		52	52.00	38.00	9.750	44.22	1.46	30.28	31.43	0.84	1.47
7	14.7	15.08		52	58.00	32.00	9.750	36.69	1.31	27.99	29.14	0.87	1.97
8	14.7	15.08		52	58.00	32.00	9.750	36.69	1.31	27.99	29.14	0.87	1.97
9	13.5	13.80		52	60.00	30.00	9.750	39.71	1.30	30.65	31.80	0.71	1.61
10	13.5	13.80		52	60.00	30.00	9.750	39.71	1.30	30.65	31.80	0.71	1.61
11	14.8	15.19		52	62.00	28.00	9.750	38.46	1.25	29.19	30.34	0.83	1.88
12	14.8	15.19		52	62.00	28.00	9.750	38.46	1.25	29.19	30.34	0.83	1.88

FIG. 3G1 and
3G1B

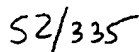


D **.arc.**

[illegible]

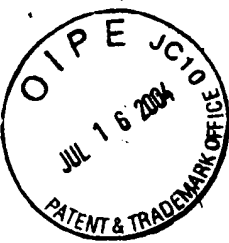
~~FIG. 3G2~~
PGS. 3G2A and 3G2B

[illegible]



~~FIG. 3I~~
FIGS. 3I1 and 3I2

[illegible]



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L .aio5_4

*** Analysis of the Focus Shift and Out-of-focus Spot Size for Converging Reference Beam ***											
(Not applicable for Stratos)											
Convergence of the reference beam:											
Focal length of parabolic mirror:											
Distance from parabolic mirror to detector:											
Per. Mirror											
Focal length											
(mm)											
Required											
foc. length											
(mm)											
Image											
distance											
(mm)											
Object											
distance											
(mm)											
Image											
distance											
(mm)											
Image											
shift											
(mm)											
Spot size											
at detector											
(mm)											
Distance (Cell E821) may have to be adjusted											
so that the maximum spot size at the detector is											
approximately the same when the 1/2 depth of field value											
is negative as it is when the 1/2 depth of field value is positive.											
(The 1/2 depth of field value is located at Cell G19)											
1	317.50	40 404.42	-14858.75	59.05	-0.95	0.64	0.58				
2	292.10	40 354.09	31841.43	58.71	-1.29	0.88					
3	322.58	40 412.89	-11928.19	59.11	-0.89	0.60					
4	292.10	40 354.09	31841.43	58.71	-1.29	0.88					
5	322.58	40 412.89	-11928.19	59.11	-0.89	0.60					
6	304.80	40 384.03	-48230.76	58.89	-1.11	0.75					
7	373.38	40 499.87	-4485.04	59.60	-0.40	0.27					
8	373.38	40 499.87	-4485.04	59.60	-0.40	0.27					
9	342.90	40 446.55	-6818.26	59.33	-0.67	0.45					
10	342.90	40 446.55	-6818.26	59.33	-0.67	0.45					
11	375.92	40 504.23	-4376.15	59.62	-0.38	0.25					
12	375.92	40 504.23	-4376.15	59.62	-0.38	0.25					

FIG. 3J
FIGS. 3J1 and 3J2



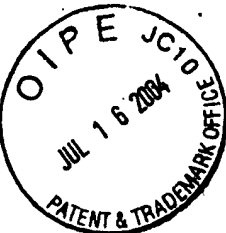
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* CDRW/IEC Calculations to Verify that the Scanner Meets the Laser Class Requirements **									
The number of overlapping lines (N-overlap) must be determined from the scanner data. A safe assumption for our scanners is to consider that two scan lines are overlapped ONLY when the difference between their diffraction angles (B) is less than 2 degrees. All else being equal, the slowest scan lines (largest angle B) will be the worst case scan lines.									
N-overlap:	1								
Motor speed (rpm):			5200						
Alpha-min (radians):			0.0015	(from standard)					
FWHM P-divergence of laser (deg.):			8	(Linked from Trmc spreadsheet)					
FWHM S-divergence of laser (deg.):			30	(Linked from Trmc spreadsheet)					
Focal length of collimating lens (mm):			6.1	(Linked from Trmc spreadsheet)					
Angle of incidence at MF plate (deg.):			29.23						
Angle of diffraction at MF plate (deg.):			42.12						
X-p (mm):			0.87						
X-s (mm):			3.93						
Average source dimension (mm):			2.40						
Distance to aperture (mm):			200	(actual distance or 200 mm, whichever is greater)					
Alpha (radians):			0.012						
C6:			7.996						
Laser power at window (mW)				tl (actual)					
Facet				7 mm transit time at actual d (seconds)					Facet count
	1	0.86	3.95856E-05	3.95856E-05	0.0000339				1
	2	0.86	3.96549E-05	3.96549E-05	0.0000341				1
	3	0.86	4.08001E-05	4.08001E-05	0.0000351				1
	4	0.86	4.08315E-05	4.08315E-05	0.0000352				1
	5	0.86	4.28115E-05	4.28115E-05	0.0000370				1
	6	0.87	4.40086E-05	4.40086E-05	0.0000381				1
	7	0.87	4.90358E-05	4.90358E-05	0.0000425				1
	8	0.87	4.90358E-05	4.90358E-05	0.0000425				1
	9	0.87	4.96126E-05	4.96126E-05	0.0000430				1
	10	0.87	4.96126E-05	4.96126E-05	0.0000430				1
	11	0.87	5.14525E-05	5.14525E-05	0.0000446				1
	12	0.87	5.14525E-05	5.14525E-05	0.0000446				1

FIG. 3L1

FIGS. 3L1A and 3L1B

FIGS. 3L2A and 3L2B

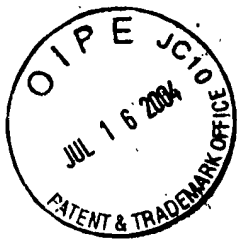


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	N	O	P	Q	R	S	T	U	V	W	X
46	Facet	1									
47	x	y	z								
48	-0.616	0.000	0.788								
49		End				Middle				End	
50	x	y	z		x	y	z		x	y	z
51	0.788	0.000	0.616		0.788	0.000	0.616		0.741	-0.367	0.582
52	-0.140	0.000	-0.990		-0.140	0.000	-0.990		-0.117	-0.367	-0.923
53	-0.595	0.448	0.667		-0.595	0.448	0.667		-0.590	0.098	0.801
54											
55											
56		Mirror 1 Corners				Mirror 2 Corners				Mirror 3 Corners	
57	x	y	z		x	y	z		x	y	z
58	3.750	-1.600	2.509		3.000	0.000	-0.112				
59	5.100	-2.400	1.728		4.800	0.000	0.382				
60	5.100	2.400	1.728		5.071	-2.256	1.066				
61	3.750	1.600	2.509		5.071	-2.256	1.066				
62					3.060	-1.000	0.175				
63											
64											
65											
66											
67											
68											
69	This station uses a split mirror for mirror #2. The second part of mirror 2 is the above										
70											
71					3.000	0.000	-0.112				
72					4.800	0.000	0.382				
73					5.071	2.256	1.066				
74					5.071	2.256	1.066				
75					3.060	1.000	0.175				
76											

FIG. 6D2

Station 2



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Z	AA	AB	AC	AD	AE	AF	AG	AH	AI	AJ
46 Facet	2									
47 x	y	z								
48 -0.616	0.000	0.788								
49	End				Middle				End	
50 x	y	z		x	y	z		x	y	z
51 0.766	0.000	0.643		0.766	0.000	0.643		0.711	-0.395	0.581
52 -0.175	0.000	-0.985		-0.175	0.000	-0.985		-0.149	-0.395	-0.907
53 -0.623	0.440	0.647		-0.623	0.440	0.647		-0.614	0.062	0.787
54										
55										
56	Mirror 1 Corners				Mirror 2 Corners				Mirror 3 Corners	
57 x	y	z		x	y	z		x	y	z
58 3.750	-1.600	2.509		3.000	0.000	-0.112				
59 5.100	-2.400	1.728		4.800	0.000	0.382				
60 5.100	2.400	1.728		5.071	-2.256	1.066				
61 3.750	1.600	2.509		5.071	-2.256	1.066				
62				3.060	-1.000	0.175				
63										
64										
65										
66										
67										
68										
69	This station uses a split mirror for mirror #2. The second part of mirror 2 is the abo									
70										
71				3.000	0.000	-0.112				
72				4.800	0.000	0.382				
73				5.071	2.256	1.066				
74				5.071	2.256	1.066				
75				3.060	1.000	0.175				
76										

FIG. 6D3

Station 2-

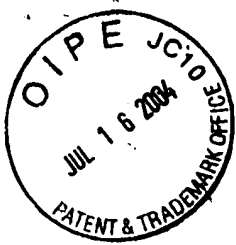


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A	B	C	D	E	F	G	H	I	J	K	L
46 Low Elevation	Facet	3									
47	x	y	z								
48 Vector from Module	-0.616	0.000	0.788								
49											
50	x	y	z								
51 Output Vectors From Disk	0.743	0.000	0.669								
52 First Mirror Reflected Directions	-0.209	0.000	-0.978								
53 Second Mirror Reflected Directions	-0.649	0.433	0.625								
54 Third Mirror Reflected Directions											
55											
56											
57	x	y	z								
58	1	3.750	-1.600	2.509							
59	2	5.100	-2.400	1.728							
60	3	5.100	2.400	1.728							
61	4	3.750	1.600	2.509							
62	5										
63	6										
64	7										
65	8										
66											
67											
68											
69 Note: Special Case!	This station uses a split mirror for mirror #2. The second part of mirror 2 is the above										
70											
71 Second Part of Mirror 2											
72											
73											
74											
75											
76											
77											

FIG. 6D4

Station 2

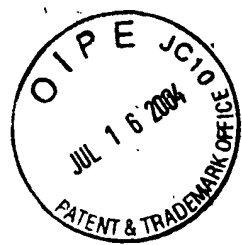


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	AL	AM	AN	AO	AP	AQ	AR	AS	AT	AU	AV
46	Facet	4									
47	x	y	z								
48	-0.616	0.000	0.788								
49	End				Middle					End	
50	x	y	z		x	y	z		x	y	z
51	0.719	0.000	0.695		0.719	0.000	0.695		0.664	-0.395	0.635
52	-0.243	0.000	-0.970		-0.243	0.000	-0.970		-0.220	-0.395	-0.892
53	-0.675	0.425	0.603		-0.675	0.425	0.603		-0.668	0.046	0.742
54											
55											
56	Mirror 1 Corners				Mirror 2 Corners				Mirror 3 Corners		
57	x	y	z		x	y	z		x	y	z
58	3.750	-1.600	2.509		3.000	0.000	-0.112				
59	5.100	-2.400	1.728		4.800	0.000	0.382				
60	5.100	2.400	1.728		5.071	-2.256	1.066				
61	3.750	1.600	2.509		5.071	-2.256	1.066				
62					3.060	-1.000	0.175				
63											
64											
65											
66											
67											
68											
69	This station uses a split mirror for mirror #2. The second part of mirror 2 is the abo										
70											
71					3.000	0.000	-0.112				
72					4.800	0.000	0.382				
73					5.071	2.256	1.066				
74					5.071	2.256	1.066				
75					3.060	1.000	0.175				
76											

FIG. 605

Station 2-

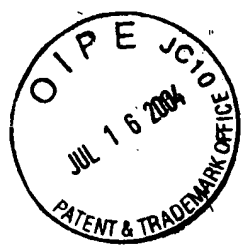


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	AX	AY	AZ	BA	BB	BC	BD	BE	BF	BG	BH
46	Facet	5									
47	x	y	z								
48	-0.616	0.000	0.788								
49		End				Middle				End	
50	x	y	z		x	y	z		x	y	z
51	0.669	0.000	0.743		0.669	0.000	0.743		0.634	-0.311	0.708
52	-0.310	0.000	-0.951		-0.310	0.000	-0.951		-0.298	-0.311	-0.903
53	-0.724	0.407	0.557		-0.724	0.407	0.557		-0.730	0.114	0.673
54											
55											
56											
57	x	y	z								
58	3.750	-1.600	2.509		3.000	0.000	-0.112				
59	5.100	-2.400	1.728		4.800	0.000	0.382				
60	5.100	2.400	1.728		5.071	-2.256	1.066				
61	3.750	1.600	2.509		5.071	-2.256	1.066				
62					3.060	-1.000	0.175				
63											
64											
65											
66											
67											
68											
69	This station uses a split mirror for mirror #2. The second part of mirror 2 is the abo										
70											
71					3.000	0.000	-0.112				
72					4.800	0.000	0.382				
73					5.071	2.256	1.066				
74					5.071	2.256	1.066				
75					3.060	1.000	0.175				
76											

FIG. 6D6

Station 2

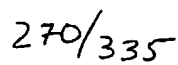


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	BJ	BK	BL	BM	BN	BO	BP	BQ	BR	BS	BT	BU	BV	BW	BX
46	Facet	6													
47	x	y	z												
48	-0.616	0.000	0.788												
49	End			Middle			End								
50	x	y	z	x	y	z	x	y	z						
51	0.616	0.000	0.788	0.616	0.000	0.788		0.596	-0.232	0.769					
52	-0.376	0.000	-0.927	-0.376	0.000	-0.927		-0.369	-0.232	-0.900					
53	-0.770	0.387	0.508	-0.770	0.387	0.508		-0.781	0.173	0.600					
54															
55															
56	Mirror 1 Corners			Mirror 2 Corners			Mirror 3 Corners								
57	x	y	z	x	y	z	x	y	z						
58	3.750	-1.600	2.509	3.000	0.000	-0.112									
59	5.100	-2.400	1.728	4.800	0.000	0.382									
60	5.100	2.400	1.728	5.071	-2.256	1.066									
61	3.750	1.600	2.509	5.071	-2.256	1.066									
62				3.060	-1.000	0.175									
63															
64															
65															
66															
67															
68															
69	This station uses a split mirror for mirror #2. The second part of mirror 2 is the above mirrored about the y axis. I.e.:														
70															
71				3.000	0.000	-0.112									
72				4.800	0.000	0.382									
73				5.071	2.256	1.066									
74				5.071	2.256	1.066									
75				3.060	1.000	0.175									
76															

FIG. 607

-Station 2



~~F/G.~~ 9 Figs. qA through qC



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Truncation analysis

Diagrams to radian conversion factor:

Truncation analysis: Effect of truncation on the diffraction limited spot size of a Gaussian beam
Given the laser and lens parameters, this spreadsheet will calculate the effect of truncation on the beam
The final result is an "effective diameter". This is an equivalent He-squared diameter that will
produce the same spot size at the focal point as the actual truncated beam. This is also the beam
diameter that will be inserted in the main scanner disk design spreadsheet.
The actual number linked to the main spreadsheet will be a rounded number.
It will usually be rounded up 0.1 to allow for tolerances.

550 Wavelength (nm)
SLD1137V8 8

20 theta-S (degrees)
Alignment (microns)

7 focal length (mm)
Numerical Aperture

0.15 Clear Aperture (mm)
Clear Aperture (mm)
(= 2 x f x NA)

1.188 He-squared beam diameter at lens (mm)

1.263 Aperture factor (m)

0.782 He-squared beam radius
(for normalised aperture)

Truncation factor: 1.219

20: 3.078
(A(Z)/A(0))^2 = 0.135335
Ln(A(Z)/A(0))^2 = -2.00000001

Effective diameter: 0.97

Spreadsheet value: 1.10

The remaining part of this spreadsheet is simply the numerical integration
of the diffraction equation for A(z) from the Mathcad program.
It includes the evaluation of the functions (A(Z)/A(0))^2 and Ln(A(Z)/A(0))^2.
It also includes a graph of (A(Z)/A(0))^2 vs Z.

delta-r	r	e ^{-j(u(r))^2}	etc.													
			A(Z1)	A(Z2)	A(Z3)	etc.	0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
0.01	0.01	0.999415	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0.02	0.02	0.998830	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0.03	0.03	0.998245	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0.04	0.04	0.997660	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0.05	0.05	0.997075	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0.06	0.06	0.996490	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0.07	0.07	0.995905	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0.08	0.08	0.995320	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0.09	0.09	0.994735	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0.1	0.1	0.994150	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0.11	0.11	0.993565	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0.12	0.12	0.992980	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0.13	0.13	0.992395	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0.14	0.14	0.991810	0	0	0	0	0	0	0	0	0	0	0	0	0	0

H = Heys; K = Kodak; P = Philips; O = GetTech
(Alternate choices - from Tom's table)

K/A337	N/A41	K/77	P/A333	P/A335	P/A337	P/777	N/A43	N/A41	P/A335	N/A51	N/A52	K/A370	G/S350	G/S350
11	10	9.5	9	8	7.5	7	6.07	6.25	6.25	6	5.4	4.6	6.1	5
0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
7.2	8	8.05	8.5	9	9.5	10	10.5	11	11.5	12	12.5	13	13.5	14
4.6	4.7	4.1	3.9	3.5	3.3	3.7	3.1	3.2	3.4	3.3	2.9	2.1	1.7	1.2

m = 1 is He-squared truncation
m > 2 is essentially no truncation

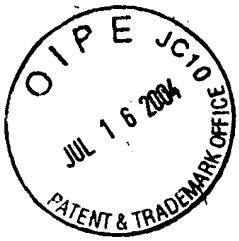
He-squared radius at focal plane is -
increased by this factor due to truncation.

To determine the effective diameter,
very 2D unit (A(Z)/A(0))^2 = 0.135335 or,
equivalently, until Ln(A(Z)/A(0))^2 = -2.
This can most easily be done by using
the SOLVER function of Excel Tools:
Target cell = \$C\$21; Value = -2
Change cell = \$C\$23

This is the effective beam diameter that
is linked to the data spreadsheet
and the main disk design spreadsheet.

FIG. 11A1

FIGS. 11A1A Through 11A1H



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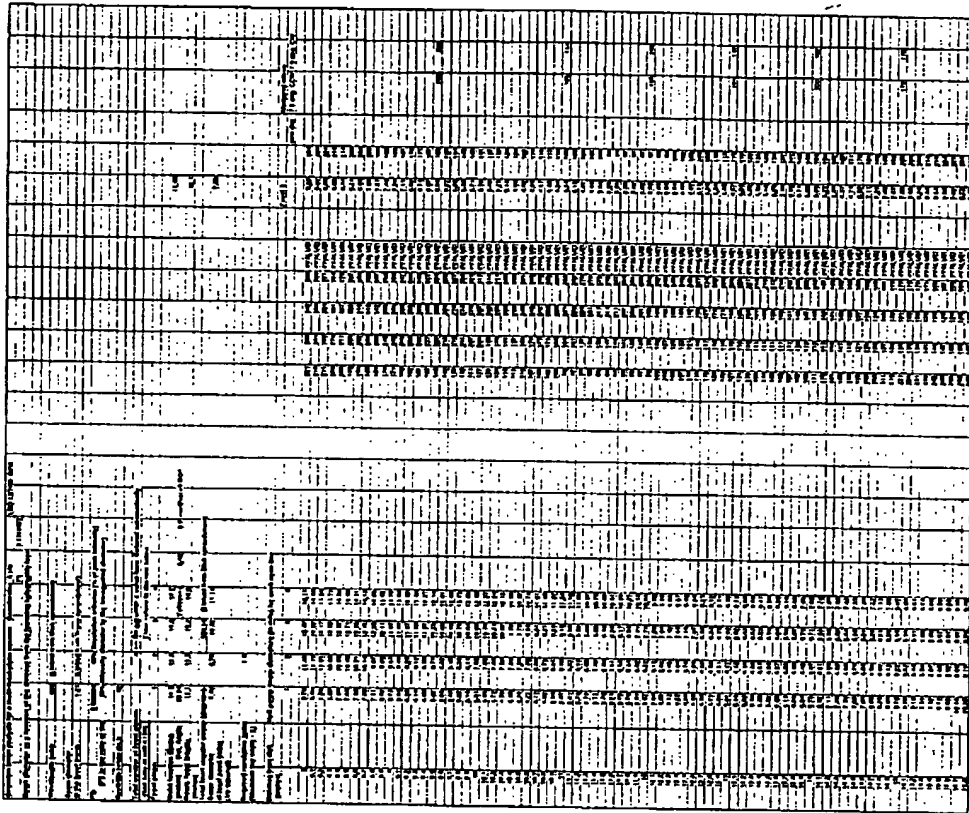
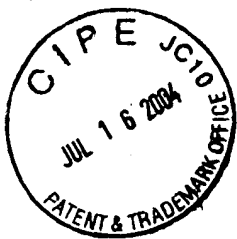
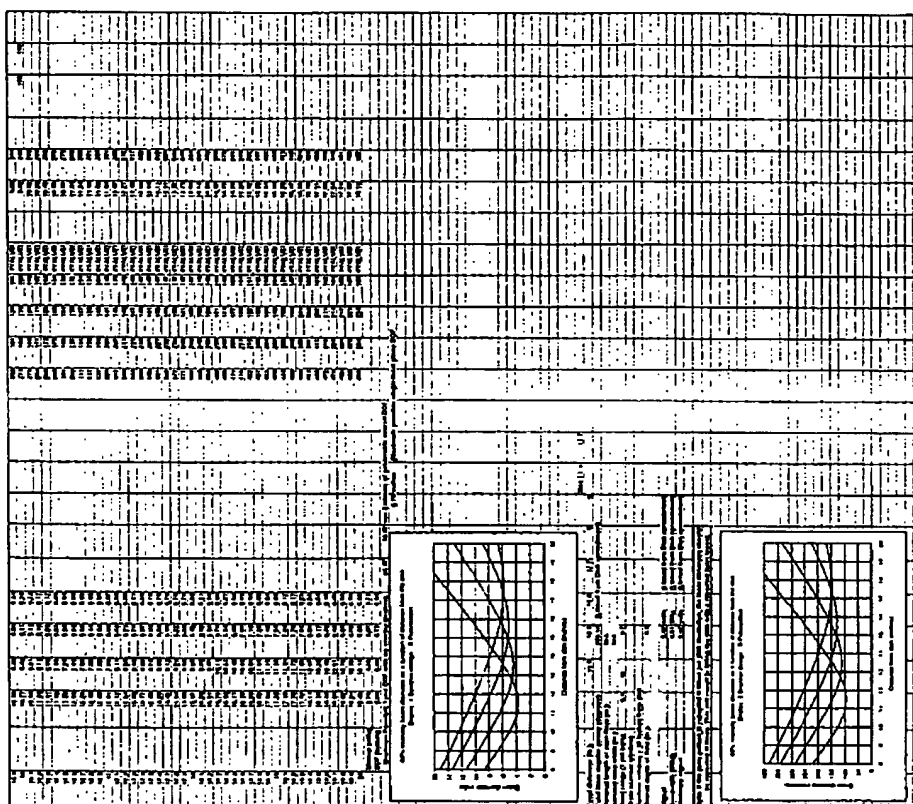


FIG. 11B1
FIGS. 11B1A through 11B1H



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~~FIG. 11B2~~



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	A	B	C	D	E	F	G	H	I	J	K	L	M
106		Facet 1											
107	G3	5.11617	1.95380	1.89155	5.01400	1.88093	1.96715	4.92433	1.81870	2.03365	4.82799	1.75935	2.10576
108	Point 1	4.98460	1.86904	1.98969	4.88136	1.79109	2.06571	4.77964	1.72960	2.14196	4.68407	1.66502	2.21298
109	Point 2	4.94695	2.08109	2.03847	4.88064	1.79549	2.06667	4.75362	1.86942	2.17507	4.68407	1.66502	2.21298
110	Point 3	4.55990	1.69707	2.31542	4.49555	1.51422	2.37191	4.31720	1.51260	2.49402	4.34215	1.44050	2.46771
111	Point 4	4.35785	1.69559	2.16575	4.28296	1.52325	2.24765	4.14486	-1.55897	2.36338	4.17995	-1.53887	2.33686
112	Point 5	4.71038	-2.01784	1.86940	4.68022	-1.80322	1.91239	4.54753	-1.91413	2.00915	4.50146	-1.76326	2.05933
113	Point 6	4.77395	-1.80620	1.83693	4.68147	-1.79883	1.91177	4.59009	-1.77513	1.98718	4.50146	-1.76326	2.05933
114	Point 7	4.89971	-1.80063	1.72862	4.80732	-1.88882	1.80291	4.72764	-1.86391	1.86903	4.83750	-1.85821	1.94186
115	Point 8	5.11617	1.95380	1.89155	5.01400	1.88093	1.96715	4.92433	1.81870	2.03365	4.82799	1.75935	2.10576
116	Point 9	5.03523	0.00000	1.78542	4.95474	0.00000	1.85000	4.87537	0.00000	1.91369	4.79689	0.00000	1.97666
117	Start of scan line	5.00607	-0.98140	1.72464	4.92129	-0.94701	1.79393	4.83778	-0.91710	1.86358	4.75656	-0.89961	1.93026
118	Middle of rotation												
119	End of scan line												
120													

FIG. 13A3 Figs. 13A3A and 13A3B

MRI

Station 1



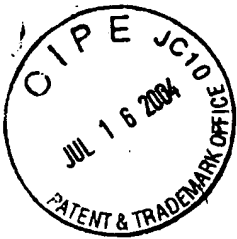
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	A	B	C	D	E	F	G	H	I	J	K	L	M
106		Facet 1			Facet 2			Facet 3			Facet 4		
107	G3	4.36645	2.65378	0.19632	4.13039	2.57939	0.16456	3.89207	2.57127	0.13136	3.63985	2.49916	0.09731
108	Point 1	4.22328	2.62785	0.17673	3.98981	2.54937	0.14541	3.72893	2.54596	0.10897	3.48464	2.46924	0.07610
109	Point 2	4.17478	2.60528	0.18686	3.98888	2.55291	0.14522	3.69351	2.66181	0.10205	3.48464	2.46924	0.07610
110	Point 3	3.78748	2.62732	0.11577	3.59353	2.46410	0.09002	3.24144	2.51989	0.04122	3.13971	2.40274	0.02698
111	Point 4	3.59708	1.89946	0.16625	3.42901	1.80124	0.14108	3.10957	1.84718	0.09716	3.03925	1.79742	0.08649
112	Point 5	4.00140	-2.16622	0.22737	3.66105	-1.97527	0.20449	3.58373	-2.08109	0.16749	3.40752	-1.93323	0.14032
113	Point 6	4.08710	-1.99138	0.23359	3.66230	-1.97181	0.20460	3.62849	-1.96992	0.17186	3.40752	-1.93323	0.14032
114	Point 7	4.22016	-2.04815	0.25597	4.01328	-2.03180	0.22675	3.80192	-2.02808	0.19711	3.57490	-1.99474	0.16470
115	Point 8	4.36645	2.65376	0.19632	4.13039	2.57939	0.16456	3.89207	2.57127	0.13136	3.63985	2.49916	0.09731
116	Point 9	4.00361	1.87032	0.21487	4.17745	1.84317	0.18369	3.94222	1.82246	0.15114	3.70025	1.80404	0.11760
117	Start of scan line	4.29670	0.23013	0.22786	4.10000	0.25000	0.20000	3.89313	0.27090	0.17070	3.67474	0.28297	0.13978
118	Middle of rotation	4.30520	-1.28070	0.25535	4.10701	-1.28788	0.22718	3.89234	-1.26997	0.19885	3.66999	-1.27078	0.16575
119	End of scan line												
120													

Fig. 13B3 Figs. 13B3A and 13B3B

MR2

Station 1



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	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S
105																			
106																			
107																			
108																			
109																			
110																			
111																			
112																			
113																			
114																			
115																			
116																			
117																			
118																			
119																			
120																			

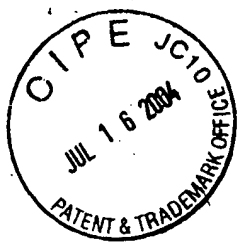
FIG. 14A1 Figs. 14A1A and 14A1B

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[illegible]

~~Fig. 14B1~~ Figs. 14B1A and 14B1B

~~Fig. 14C1~~ Figs. 14C1A and 14C1B

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	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S
106		Facet 1			Facet 2			Facet 3			Facet 4			Facet 5			Facet 6		
107	03	7.39433	0.36621	3.60327	2.31835	0.35437	3.81836	2.23112	0.36203	4.03445	7.17887	0.35054	4.26573	7.03506	0.35881	4.74102	6.87159	0.34312	5.26344
108		Point 1	0.36621	3.60327	2.31835	0.35437	3.81836	2.23112	0.36203	4.03445	7.17887	0.35054	4.26573	7.03506	0.35881	4.74102	6.87159	0.34312	5.26344
109		Point 2	0.36621	3.60327	2.31835	0.35437	3.81836	2.23112	0.36203	4.03445	7.17887	0.35054	4.26573	7.03506	0.35881	4.74102	6.87159	0.34312	5.26344
110		Point 3	0.36621	3.60327	2.31835	0.35437	3.81836	2.23112	0.36203	4.03445	7.17887	0.35054	4.26573	7.03506	0.35881	4.74102	6.87159	0.34312	5.26344
111		Point 4	0.36621	3.60327	2.31835	0.35437	3.81836	2.23112	0.36203	4.03445	7.17887	0.35054	4.26573	7.03506	0.35881	4.74102	6.87159	0.34312	5.26344
112		Point 5	0.36621	3.60327	2.31835	0.35437	3.81836	2.23112	0.36203	4.03445	7.17887	0.35054	4.26573	7.03506	0.35881	4.74102	6.87159	0.34312	5.26344
113		Point 6	0.36621	3.60327	2.31835	0.35437	3.81836	2.23112	0.36203	4.03445	7.17887	0.35054	4.26573	7.03506	0.35881	4.74102	6.87159	0.34312	5.26344
114		Point 7	0.36621	3.60327	2.31835	0.35437	3.81836	2.23112	0.36203	4.03445	7.17887	0.35054	4.26573	7.03506	0.35881	4.74102	6.87159	0.34312	5.26344
115		Point 8	0.36621	3.60327	2.31835	0.35437	3.81836	2.23112	0.36203	4.03445	7.17887	0.35054	4.26573	7.03506	0.35881	4.74102	6.87159	0.34312	5.26344
116		Point 9	0.36621	3.60327	2.31835	0.35437	3.81836	2.23112	0.36203	4.03445	7.17887	0.35054	4.26573	7.03506	0.35881	4.74102	6.87159	0.34312	5.26344
117		Start of scan line	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
118		Middle of scan line	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
119		End of scan line	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
120																			

FIG. 15A3
FIGS. 15A3A and 15A3B

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[illegible]

~~F1G. 15C3~~

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~~Fig. 15D3~~ Figs. 15D3A and 15D3B

A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S
105	107	103																
Point 1	7.34943	0.36027	7.31858	7.31858	0.34347	3.81898	7.28212	0.36293	4.02445	7.17897	0.33054	4.26373	7.05008	0.33981	4.74102	8.87108	0.34312	5.26344
Point 2	7.35669	0.30877	7.27018	7.27018	0.29548	3.83889	7.20014	0.30030	4.16642	7.13000	0.29182	4.36786	6.97884	0.30018	4.86653	8.81701	0.28708	5.40885
Point 3	7.35083	0.43214	7.37848	0.29830	0.39365	3.93374	7.20960	0.36665	4.19784	7.13000	0.29182	4.36786	6.97884	0.30018	4.86653	8.81701	0.28708	5.40885
Point 4	7.19688	0.19089	0.05895	7.19493	0.17837	3.82687	7.04902	0.16476	4.07132	7.02005	0.13884	4.89313	6.81286	0.12488	5.31704	8.72143	0.18544	5.54778
Point 5	6.78106	-2.71194	3.93330	6.88288	-2.84072	3.83654	6.61109	-2.72068	4.17238	6.84131	-2.87541	4.23771	6.28745	-2.80040	4.82441	6.22148	-3.08048	5.26668
Point 6	6.82315	-2.81744	3.95139	6.78588	-2.85719	3.81184	6.68206	-2.86857	4.30074	6.82659	-2.93554	4.27771	6.28745	-2.80041	4.82441	6.22148	-3.08048	5.26668
Point 7	6.88196	2.70439	3.33025	6.77043	2.94482	3.41138	6.78118	2.78811	3.78090	6.81888	3.06818	3.96892	6.47746	2.91719	4.48112	6.28421	3.12602	4.86548
Point 8	6.85448	-2.80489	3.21407	6.78682	-2.89436	3.40022	6.75002	-2.83000	4.34975	6.84612	-3.06818	4.26373	6.47746	-2.91719	4.48112	6.28421	-3.12602	4.86548
Point 9	7.38483	0.36421	7.31635	7.31635	0.35437	3.81836	7.25212	0.36782	4.03445	7.17887	0.33004	4.28373	7.03008	0.33981	4.74102	8.87158	0.34312	5.26344
Start of main line	7.32381	0.00361	7.31749	7.25800	0.00056	3.78942	7.18248	0.00004	4.00001	7.15289	-0.00002	4.22381	6.97602	0.00007	4.85960	8.82144	0.00008	5.21121
Middle of rotation	7.32225	0.00000	3.97381	7.19245	0.00000	3.78533	7.18245	0.00000	4.00000	7.15289	0.00000	4.22382	6.97601	0.00000	4.85960	8.82143	0.00000	5.21120
End of main line	7.31771	-2.11473	3.34372	6.62439	-2.13440	3.41071	6.67815	-2.14504	3.68387	6.77389	-2.39463	4.23384	6.63430	-2.20763	4.33960	6.44831	-2.50435	4.84745